

**Handout: Channel Flow - Mean Velocity Profiles****Similarity**

$$\langle U \rangle = f(\rho, \nu, \delta, y, \frac{dp_w}{dx}) = f(\rho, \nu, \delta, y, u_\tau)$$

$\Rightarrow 6 - 3 = 3$  non-dimensional groups

$$\frac{\langle U \rangle}{u_\tau} = f\left(\frac{y}{\delta}, \frac{\delta}{\delta_\nu}\right) = f\left(\frac{y}{\delta}, \text{Re}_\tau\right)$$

One can do the same analysis for the Velocity Gradient:

$$\frac{d\langle U \rangle}{dy} = \frac{u_\tau}{y} \Phi\left(\frac{y}{\delta}, \frac{y}{\delta_\nu}\right)$$

$\delta_\nu$  is the appropriate length scale in the viscous wall region, while  $\delta$  is the appropriate length scale in the outer layer

**The law of the wall**

Prandtl (1925): In the inner layer ( $y/\delta \ll 1$ ) and at high Reynolds numbers  $\langle U \rangle$  is determined only by the viscous scales

$$\Rightarrow \frac{d\langle U \rangle}{dy} = \frac{u_\tau}{y} \Phi_I\left(\frac{y}{\delta_\nu}\right) \quad \text{for } y/\delta \ll 1 \quad (1)$$

with

$$u^+ = \frac{\langle U \rangle}{u_\tau} \quad \text{and} \quad y^+ = \frac{y}{\delta_\nu}$$

$$\Rightarrow \frac{du^+}{dy^+} = \frac{1}{y^+} \Phi_I(y^+) \quad (2)$$

The integral of the previous equation is the **Law of the Wall** valid in viscous sublayer and the inner layer ( $y/d < 0.1$ )

$$u^+ = f_w(y^+) \quad (3)$$

where

$$f_w(y^+) = \int_0^{y^+} \frac{1}{y^+} \Phi_I(y^+) dy^+$$

### Viscous Sublayer

From equation (3)

$$f_w = u^+ = \frac{\langle U \rangle}{u_\tau}$$

$$\Rightarrow f_w(0) = 0$$

$$f_w'(0) = \left. \frac{du^+}{dy^+} \right|_{y=0}$$

$$= \frac{\delta_v}{u_\tau} \left. \frac{\partial \langle U \rangle}{\partial y} \right|_{y=0}$$

$$= \frac{\nu}{u_\tau^2} \frac{\tau_w}{\rho \nu}$$

$$= \frac{\rho}{\tau_w} \frac{\tau_w}{\rho} = 1$$

Hence, the Taylor series expansion for small  $y^+$

$$u^+ = f_w(y^+) = f_w(0) + f_w'(0)y^+ + O(y^{+2})$$

$$\Rightarrow u^+ = y^+$$

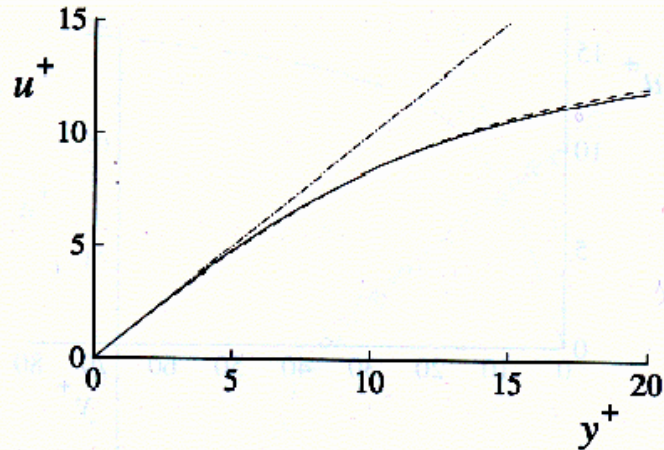


Fig. 7.5. Near-wall profiles of mean velocity from the DNS data of Kim *et al.* (1987): dashed line,  $Re = 5,600$ ; solid line,  $Re = 13,750$ ; dot-dashed line,  $u^+ = y^+$ .

### The Log Law

At large Reynolds numbers, the outer part of the inner layer corresponds to large  $y^+$  where viscosity has little effect ( $\Phi$  independent of  $\frac{y}{\delta_v}$ )

$$\Phi = \Phi\left(\frac{y}{\delta_v}, \frac{y}{\delta}\right)$$

$$y^+ \gg 1 \Rightarrow \frac{y}{\delta_v} = \frac{y}{\delta} \frac{\delta}{\delta_v} \gg 1$$

$$\Rightarrow \frac{y}{\delta} \gg \frac{\delta_v}{\delta} = \frac{\nu}{u_\tau \delta} = Re_\tau^{-1}$$

Also  $\Phi$  independent of  $\frac{y}{\delta}$  for

$$\frac{y}{\delta} \ll 1 \quad \text{let's say} \quad \frac{y}{\delta} < 0.1$$

$$\Rightarrow \frac{y}{\delta_v} \frac{\delta_v}{\delta} < 0.1$$

$$\Rightarrow y^+ < 0.1 \frac{\delta}{\delta_v} = 0.1 \frac{\delta u_\tau}{\nu} = 0.1 Re_\tau$$

where the edge of the inner layer was defined at  $0.1\delta$ .

So if  $Re_\tau$  is such that  $\frac{y}{\delta} \gg Re_\tau^{-1}$  and  $y^+ = y/\delta_v < 0.1Re_\tau$

$\Phi_I(y^+)$  independent of both  $\frac{y}{\delta_v}$  (viscosity) and of  $\frac{y}{\delta}$ , thus from equation (2):

$$\begin{aligned} \Rightarrow \Phi_I &= const = \frac{1}{\kappa} \\ \Rightarrow \frac{du^+}{dy^+} &= \frac{1}{\kappa y^+} \\ \Rightarrow u^+ &= \frac{1}{\kappa} \ln y^+ + B \end{aligned}$$

with

$\kappa = 0.41$  (Von Karman constant)

$B=5.2$

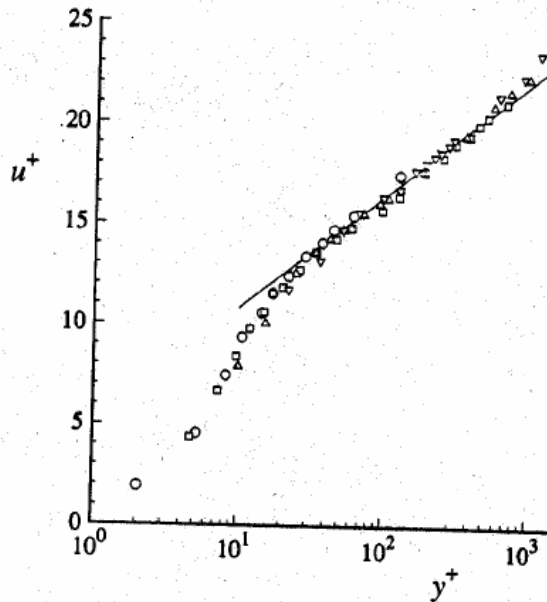


Fig. 7.7. Mean velocity profiles in fully developed turbulent channel flow measured by Wei and Willmarth (1989):  $\circ$ ,  $Re_0 = 2,970$ ;  $\square$ ,  $Re_0 = 14,914$ ;  $\Delta$ ,  $Re_0 = 22,776$ ;  $\nabla$ ,  $Re_0 = 39,582$ ; line, the log law, Eqs. (7.43)–(7.44).

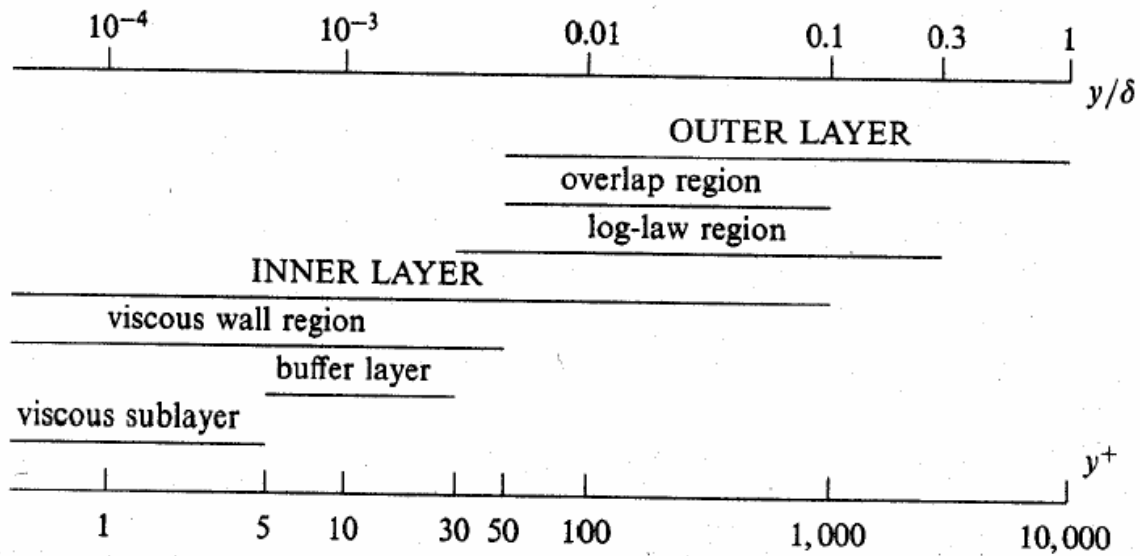


Fig. 7.8. A sketch showing the various wall regions and layers defined in terms of  $y^+ = y/\delta_v$ , and  $y/\delta$ , for turbulent channel flow at high Reynolds number ( $Re_\tau = 10^4$ ).

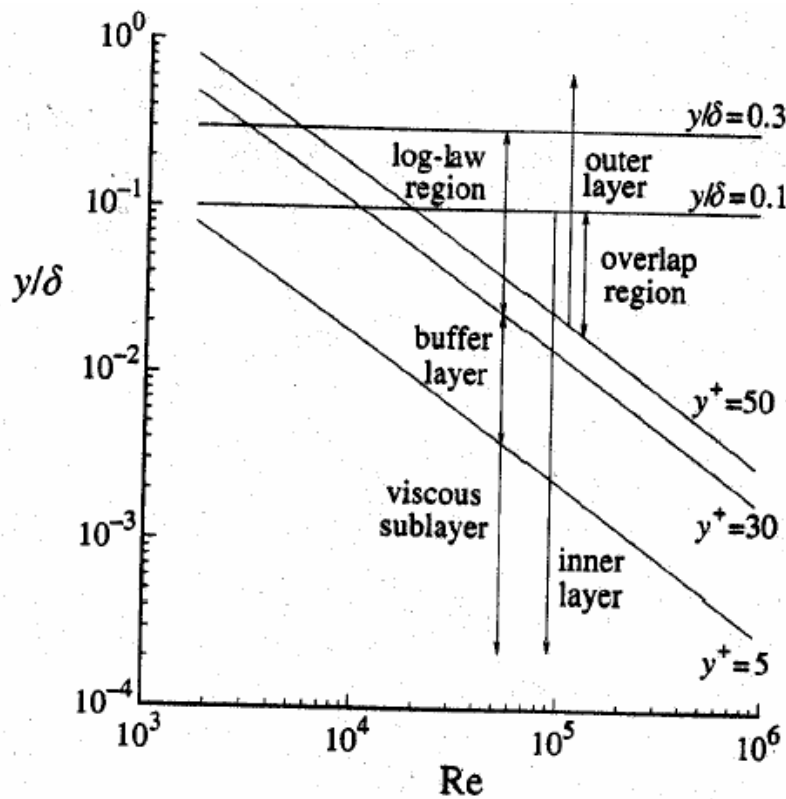


Fig. 7.13. Regions and layers in turbulent channel flow as functions of the Reynolds number.

## Velocity Defect Law

In the outer layer ( $y^+ > 50$ ) the assumption that  $\Phi$  is independent of  $v$  implies that, for large  $y/\delta_v$ ,  $\Phi$  tends asymptotically to a function of  $y/\delta$  only:

$$\frac{d\langle U \rangle}{dy} = \frac{u_\tau}{y} \Phi_0\left(\frac{y}{\delta}\right) \quad (4)$$

By integrating in  $y$  from  $y$  to  $\delta$  (channel centerline)

$$\int_y^\delta \frac{d\langle U \rangle}{dy'} dy' = \int_y^\delta \frac{u_\tau}{y'} \Phi_0\left(\frac{y'}{\delta}\right) dy'$$

$$\frac{U_0 - \langle U \rangle}{u_\tau} = F_D\left(\frac{y}{\delta}\right) \quad \text{with} \quad F_D\left(\frac{y}{\delta}\right) = \int_{y/\delta}^1 \frac{1}{y'} \Phi_0(y') dy' \quad (5)$$

Unlike the law of the wall function  $f_w(y^+)$  which is universal, the function  $F_D\left(\frac{y}{\delta}\right)$  is different in different flows.

At sufficiently high Reynolds numbers (approximately  $Re > 20,000$ ) there is an overlap region between the inner layer and the outer layer (see Figs. 7.8 and 7.13). In this region both equations (1) and (4) are valid

$$\frac{y}{u_\tau} \frac{d\langle U \rangle}{dy} = \Phi_I\left(\frac{y}{\delta_v}\right) = \Phi_0\left(\frac{y}{\delta}\right) \quad \text{for} \quad \delta_v \ll y \ll \delta$$

This can be satisfied only if the two functions on the right hand side are equal to the same constant ( $1/\kappa$ ), which leads to

$$\Rightarrow \frac{d\langle U \rangle}{dy} = \frac{u_\tau}{y\kappa} \quad \text{for} \quad \delta_v \ll y \ll \delta$$

For small  $y/\delta$ , the velocity defect law (equation 5) can be written as:

$$\frac{U_0 - \langle U \rangle}{u_\tau} = F_D\left(\frac{y}{\delta}\right) = -\frac{1}{\kappa} \ln \frac{y}{\delta} + B_1 \quad (6)$$

The value of the flow-dependent constant  $B_1$  is  $\sim 0.2$  based on DNS and  $\sim 0.7$  based on experimental data for channel flows.

**Statistics in turbulent channel flows:**

Table 7.2. *Statistics in turbulent channel flow, obtained from the DNS data of Kim et al. (1987),  $Re = 13,750$*

	Location		
	Peak production $y^+ = 11.8$	Log law $y^+ = 98$	Centerline $y^+ = 395$
$\langle u^2 \rangle / k$	1.70	1.02	0.84
$\langle v^2 \rangle / k$	0.04	0.39	0.57
$\langle w^2 \rangle / k$	0.26	0.59	0.59
$\langle uv \rangle / k$	-0.116	-0.285	0
$\rho_{uw}$	-0.44	-0.45	0
$Sk/\varepsilon$	15.6	3.2	0
$\mathcal{P}/\varepsilon$	1.81	0.91	0

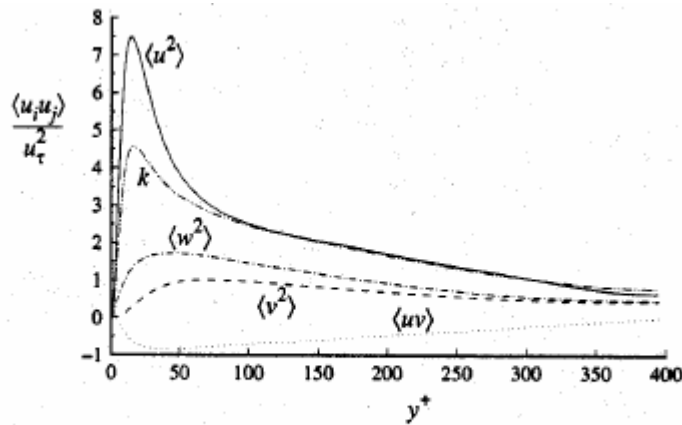


Fig. 7.14. Reynolds stresses and kinetic energy normalized by the friction velocity against  $y^+$  from DNS of channel flow at  $Re = 13,750$  (Kim et al. 1987).

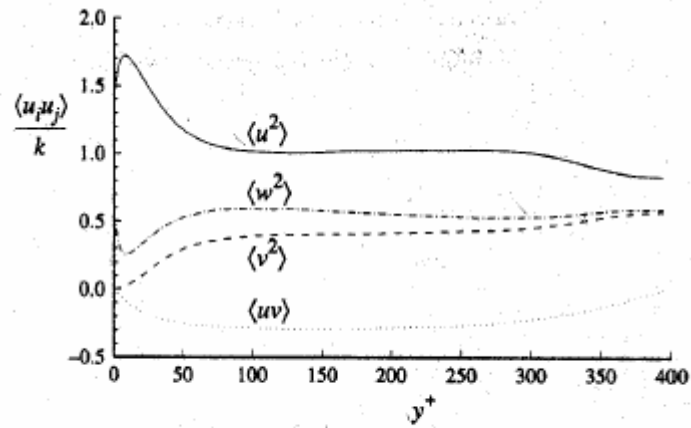


Fig. 7.15. Profiles of Reynolds stresses normalized by the turbulent kinetic energy from DNS of channel flow at  $Re = 13,750$  (Kim *et al.* 1987).

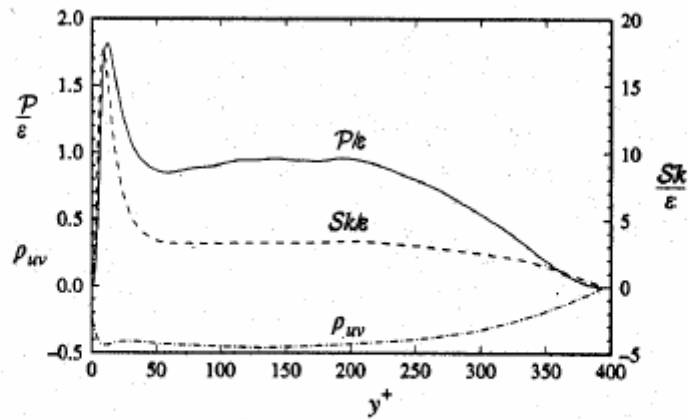


Fig. 7.16. Profiles of the ratio of production to dissipation ( $P/\epsilon$ ), normalized mean shear rate ( $Sk/\epsilon$ ), and shear stress correlation coefficient ( $\rho_{uv}$ ) from DNS of channel flow at  $Re = 13,750$  (Kim *et al.* 1987).



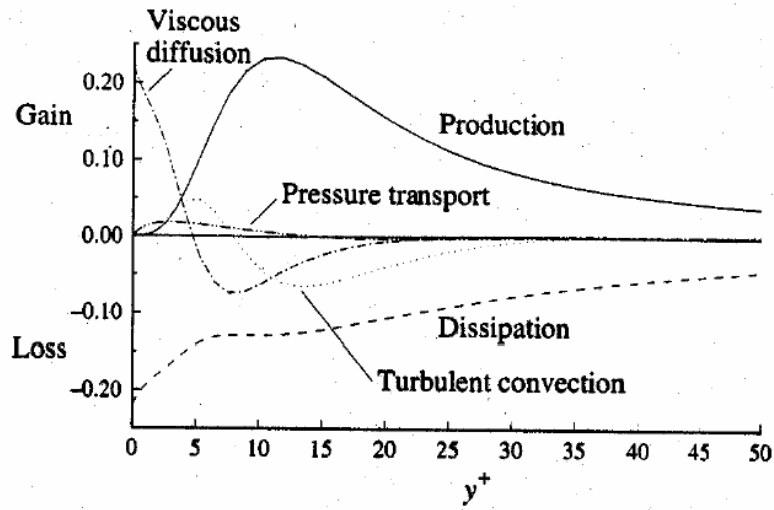


Fig. 7.18. The turbulent-kinetic-energy budget in the viscous wall region of channel flow: terms in Eq. (7.64) normalized by viscous scales. From the DNS data of Kim *et al.* (1987).  $Re = 13,750$ .